Industry Meeting Resolutions

Meeting Date: August 8, 2008
Meeting Venue: Phone-Conference
In Attendance: N. Hawkins, Y. Kurama, B. Smith

The following resolutions have been made based on the meeting:

Test Specimen Design

- The confinement steel design for the first test specimen as well as the application of ACI ITG 5.2, Table 5.6.3.9 were reviewed and approved.
- The confinement steel reinforcement will be ASTM A706. This will allow for better ductility of the confinement steel.
- For the calculation of the maximum validation drift (per ACI ITG 5.1, Equation 1) and the calculation of $L_p$ (i.e., the effective height of the plastic hinge zone at the toe of the wall, per ACI ITG 5.2, Section 5.6.3.10), $h_w$ will be taken as the total height of the wall and not the height to the applied load.
- The confinement steel spacing within the scaled test specimens will satisfy ACI 318-08, Section 21.4.6.3, which limits the maximum spacing of the confinement steel to 25% of the wall thickness. For this calculation, the wall thickness will be taken as the unscaled wall thickness, since the aggregate size of the concrete used in the test specimens will be unscaled.
- The preferred failure modes of the test specimens beyond the maximum validation drift are the ductile fracture of the energy dissipating mild steel reinforcement or the crushing of the confined concrete. Undesirable failure modes include the fracture of the PT steel, shear failure of the wall panels, and shear slip at the horizontal wall panel joints.